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PATENT SPECIFICATION



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COMPLETE SPECIFICATION

Improvements in or relating to Optical Lens Systems

We, Ernst Leitz G.m.b.H., of Wetzlar, Germany, a German Company, do hereby declare the nature of this invention and in what manner the same is to be performed, to be particularly described and ascertained in and by the following statement:—

The present invention relates to a specific variety of the so-called triplet type of lens system, which, in its simplest form, consists of two collecting members enclosing a biconcave dispersing member.

Many varieties of this type are known which have been obtained by inserting 15 cemented surfaces in the members and/or by subdividing one or more members each into two. The present invention relates to that variety in which a dispersing meniscus member, the outer surfaces of 20 which are convex towards the object side, is arranged between the first collecting member (the numbering being reckoned from the object side) and the biconcave dispersing member. The first two members 25 of such an optical system form a partial system after the fashion of a Gauss optical system, whereas the following members still clearly indicate a triplet origin. Optical systems of this type are known having in the dispersing meniscus member a highly-dispersive cemented surface which is required not only for the chromatic correction of the optical system, but very essentially also for its spherical correction.

It is an object of the present invention to remove or at least diminish the considerable spherical zone which such systems show at great rapidity, and also the astigmatic zone which arises at a large image angle in such systems, as well as the distortion errors. The "spherical zone" and "astigmatic zone" of a corrected system are those zones at which the spherical or astigmatic corrections respectively are substantially worse than they are in the centre and margin of the image field.

Our investigations have shown that in 50 optical systems of this type, which in themselves allow of combining the properties of a Gauss optical system with those of a triplet in an advantageous manner,

substantial improvements in the direction indicated are obtained if the cemented 55 surface in the dispersing meniscus member no longer contributes to a great extent to the spherical correction, but for this correction, chiefly the opposed air-exposed concave surfaces of the meniscus member 60 and the biconcave dispersing member are used. The cemented surface of the meniscus member is relieved of the spherical correction so far that the absolute effect of this cemented surface on 65 the spherical aberration becomes the smallest of those of all the three surfaces of the meniscus member. Furthermore, the surface of the biconcave member on the image side has such a curvature that 70 this surface contributes not more than numerically about 20% to the total refractive power of the system. Under these conditions, and if a collecting cemented surface which is concave towards the 75 object side is inserted in the biconcave member, the spherical zone errors can be kept small to a great extent, while distortion and appreciable astigmatic intermediate errors are substantially avoided 80 and the Petzval sum is small.

Preferably in both the meniscus and biconcave members, the lens of the glass with a higher Abbé V number, seen from the object side, stands in front of the lens 85 of the glass with a smaller Abbé V number.

Whether in a particular case the biconcave dispersing member is followed by only one or two converging members depends upon the specific requirements which are made with regard to the rapidity and to the image angle, and is a matter familiar to any person skilled in the art. Likewise, besides the cemented surfaces in the meniscus and biconcave members, already mentioned, additional cemented surfaces may be provided in the collecting members.

An embodiment of the invention is 100 illustrated diagrammatically, by way of example, in the accompanying drawing. L_1 indicates the first collecting member of thickness d_1 , having two air-exposed surfaces r_1 , r_2 , L_2 and L_3 indicate two 105 lenses cemented together along the surface

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r₄ and forming the meniscus member which has the air-exposed surfaces r₃ and r₅, the thicknesses of the lenses L₂ and L₃ are d₂ and d₃ respectively. The distance 5 of the meniscus member from the collecting member L₁ is A₁. L₄ and L₅ indicate two lenses cemented together along the surface r₇ and forming the biconcave dispersing member which has the air-10 exposed surfaces r₆ and r₈. The thicknesses of the lenses L₄ and L₅ are d₄ and d₅ respectively. The distance of the biconcave dispersing member from the meniscus member is A₂. L₆ indicates a 15 collecting lens having the air-exposed surfaces r₉ and r₁₀. The thickness of the lens L₄ is d₆, its distance from the bicon-

cave dispersing member being A_3 . L_7 indicates a further collecting lens having the air-exposed surfaces r_{11} and r_{12} . The 20 thickness of the lens L_7 is d_7 and its distance from the lens L_6 is A_4 .

The specification of this lens system is since in the following table.

The specification of this lens system is given in the following table which is believed to be self-explanatory. A, B, I', 25 P and ☐ are the Seidel partial coefficients according to the textbook of M. Berek, Grundlagen der praktischen Optik, Berlin, 1930, pages 61—71, their totals being indicated by S_I, S_{II}, S_{II}, 30 S_{II}, S_V respectively. In column 4 the material is defined by its mean refractive index, denoted by n. The Abbé V number is also given.

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TABLE

			•	-		
	Surface.	Curvature.	Thicknesses and distances.	${f Medium}$		Proportion of the refractive power.
				n	V	
40	r_1	+1.731	7 0 100	1.564	61	+0.63
	r_{2} .	+0.191	$d_1 = 0.108$	•		+0.25
	$r_{\scriptscriptstyle 3}$	+3.221	$A_1 = 0.003$	Air		+0.81
	r_4	+1.442	$d_2 = 0.108$	1.620	60	-0.02
	$r_{\mathfrak{s}}$	+4.587	$d_{\rm \tilde{a}}\!=\!0.042$	1.673	32	-0.97
50	$r_{\scriptscriptstyle \mathrm{G}}$	-3.033	$A_2 = 0.193$	Air		-0.87
	r_7	-4.401	$d_4 = 0.069$	1.592	58	+0.09
	r ₈	+0.175	$d_{\rm s}\!=\!0.031$	1.533	49	-0.10
55		-0.081	$A_a = 0.008$	Air	•	+0.05
	r_{9}		$d_{\rm s}\!=\!0.058$	1.620	60	+0.57
60	$r_{\mathfrak{10}}$	-1.855	$A_4 = 0.003$	Air	•	+0.03
	r_{11}	+0.908	$d_z\!=\!0.081$	1.620	60	+ 0.53
	$r_{\scriptscriptstyle 12}$	-0.742			Tota	
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		A	В	$f \Gamma$	P		
		+1.19	+0.69	+ 0.40	+0.62	+0.59	
		+0.22	-0.32	+0.46	-0.07	-0.58	
		+0.69	+0.41 .	+0.24	+1.23	+0.86	
5		-0.03	+0.04	- 0.05	+0.03	+0.02	
		-1.17	-0.98	-0.82	-1.85	-2.23	
		-2.41	+0.09	- 0.00	-1.13	+0.04	
		+0.38	+0.15	+0.06	+0.11	+0.06	
		-0.01	-0.04	-0.30	-0.06	-2.67	
10		+0.00	+0.02	+0.21	-0.03	+2.53	
		+0.65	-0.06	+ 0.01	+0.71	-0.07	
		-0.00	-0.01	-0.29	+0.35	+1.41	
		+0.73	-0.07	+ 0.01	+0.28	-0.03	
		S_r	S_{m}	S_{rrr}	Szy	S_v	
15	Totals	+0.24	-0.08	- 0.07	+0.19	-0.07	

The lens system in the example given can easily be finely corrected to furnish a system of great rapidity and having a comparatively large image angle.

Having now particularly described and ascertained the nature of our said invention and in what manner the same is to be performed, we declare that what we claim is:—

1. A rapid optical lens system, the first three members of which are respectively a collecting member, a dispersing meniscus member the air-exposed surfaces of which are convex towards the object side, and a biconcave dispersing member, these members being followed by one or two converging members, and a cemented surface being provided at least in each of the meniscus and biconcave members, characterised in that the absolute effect of the cemented surface in the meniscus member on the spherical aberrations, is the smallest of those of all the three surfaces

of the meniscus member; the surface of the biconcave member on the image side 40 has such a curvature that this surface contributes not more than numerically about 20% to the total refractive power of the system and the cemented surface in the biconcave member is collecting and concave towards the object side.

2. A rapid optical lens system as claimed in claim 1, wherein in both the meniscus and biconcave members, the lens of the glass with a higher Abbé V number, 50 seen from the object side, stands in front of the lens of the glass with a smaller Abbé V number.

3. A rapid optical lens system substantially as herein described with reference 55 to the example illustrated in the accompanying drawing.

Dated this 11th day of June, 1937.

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